

SMART Portal 2D

Designing open sided building frames



Version: 1.0



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Revision history

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1 Introduction

The current versions of SMART Portal 2D and 3D are configured so as to ease the input of data for portal framed buildings with closed sides. In order to deal with open sided buildings the default wind pressure and suction coefficients must be edited and this requires careful thought. This guide aims to help with this by providing commentary on the relevant code clauses and worked examples. The guide has been written specifically for SMART Portal 2D but is equally applicable to the main frames in SMART Portal 3D. Further guidance or user interpretation may be required for application to the design of purlins, sheeting rails and end frames in SMART Portal 3D. This document may be superseded in due course by specific software support for buildings with open sides.

Pending the release of the Eurocode version of CADS SMART Portal software it is assumed that for the time being, users will refer to the design standards BS 5950-1:2000 and BS 6399-1, 2 and 3 and this temporary guide has been prepared accordingly.

This guide has been prepared with appropriate professional engineering logic and care but it has no official status and its interpretation and application is the responsibility of the user.

2 Relevant BS 6399-2 clauses and tables

The following cases of open sided portal framed buildings can be identified:

- One side open which may be a left, right, near or far side in the SMART Portal convention
- Two adjacent sides open there are four possible configurations
- Two opposite sides open two possible configurations
- Three sides open four possible configurations
- Four sides open

BS 6399-2 treats the 'four sides open' case as a canopy and in section 2.5.9.1 gives roof net pressure coefficients in Table 13 for monopitch canopies and table 14 for duopitch canopies. The tables include for fully open and blocked conditions. Multi-span canopies are treated by applying reduction factors to the coefficients for downwind spans according to Table 15.

BS 6399-2 section 2.6.3 requires the other cases of open sides to be treated as enclosed buildings in respect of external pressure coefficients but provides special internal pressure coefficients in Table 18.

A grandstand may fall into either of the above categories depending upon the configuration of its back and side walls if present ie whether they are they full or part height and whether they are supported by the main frames.

Rather than comment further on the text of BS 6399-2 it is proposed to consider some worked examples using SMART Portal in the following sections of this guide. Each example considers one configuration of open sides for a single span building. Common text is repeated between examples in order to avoid the need for cross referencing and interpretation. It is therefore necessary to read only the part of section 3 applicable to the configuration of interest.

Note that it is not necessary for side cladding to be entirely absent for a side to be considered open. One normal sized open bay is more than sufficient to provide the requisite airflow. Smaller



permanent or accidental openings may be worth considering as `dominant openings' under section 2.6.2 of BS 6399-2.

Where the whole side is not fully open but only some bays there are two design conditions to be addressed:

- Frames where the open side column is free standing thereby sustaining negligible direct wind load.
- Frames where the open side column supports attached cladding thereby sustaining direct wind load.

The 17 examples are listed and their wall configurations are shown diagrammatically in plan as follows:

Example 1	All sides clad		
			-

Example 2 Left side partly/fully open

Example 4 Near side fully/partly open

Right side fully/partly open



Example 3

	_	_
	_	

Example 5 Far side fully/partly open

Example 6 Near and left sides fully/partly open

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Example 7 Near and right sides fully/partly open

Example 8 Far and left sides fully/partly open

Far and right sides fully/partly open



Example 9

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Example 10	Near and far sides	fully/partly open
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	Left and right	il sides i di	v/bartiv oper
			<i>// P · · / · P · ·</i>

European la 12	Non- for and left states fully from the surger
Example 12	Near, far and left sides fully/partly open

Example 13	Near, far and right sides fully/partly open
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Example 14	Near, left and right sides fully/partly open
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Example 15 Far, left and right sides fully/partly open

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Example 16 All sides fully/partly open

Example 17 All sides fully open (canopy)

For instructions on editing the default wind parameters given in section 3.1 refer to the relevant section 3.23.17 below for the building proposed. It is not necessary to read the other sections. Note that the wind pressure coefficients given in the examples are for the given frame dimensions and different values of the external wind coefficients may result from interpolating in the relevant tables for a particular building design.

Finally it may be noted that for main frame design the most onerous wind condition arises when either the left or right side column supports cladding and the other column is freestanding.



3 Worked examples

3.1 Duopitch portal frame building with all sides clad

This example is the benchmark or reference frame against which open sided variations may be compared. It consists of a symmetrical single 20 m span building with 5 degree pitch roof and 5.0 m eaves height. There are 6 no 6.0 m bays. For simplicity the effective wind speed is taken as 35 m/s in all directions. This produces a wind-critical design for this building with closed sides and 10% fixity base connections whereas 30 m/s does not.

The following screenshots show the wind parameter input pages with default coefficients for the case of a building with closed sides.

Wind parameters - BS6399 pt2 Accept or edit the general parameters applicable for the entire building					
Wind Blowing From	Left	Right	Near	Far	^
Effective Wind Speed (Ve)	35.000	35.000	35.000	35.000	
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	Ξ
Internal Surface Coefficients					
Internal Size Effect Factor Ca	0.739	0.739	0.739	0.739	
Basic Pressure Coefficient	0.200	0.200	0.200	0.200	
Factored Pressure Coefficient	0.152	0.152	0.152	0.152	
Basic Suction Coefficient	-0.300	-0.300	-0.300	-0.300	-
Analysis Mode Standard O Hybrid Restore Current Restore All					

Fig 1.1 Internal surface coefficients

Wind Load - BS6399pt2-Span 1

Accept or edit the member wind loading parameters for the specific span.

Wind Blowing From	Left	Right	Near	Far	Ľ
	Left Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	11
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500	1 1
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497	1
	Right Wall/Co	olumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	1
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	1.

Fig 1.2 Left and right wall external surface coefficients



Wind Blowing From	Left	Right	Near	Far	-
	Left Roof/Ra	after	, 		
Size Effect Factor Ca	0.936	0.936	0.936	0.936	
Basic Main Zone Coefficient	-0.600	-0.400	-0.600	-0.500	
Basic Edge Zone Coefficient	-1.800	-0.900	-0.600	-0.500	Ξ
Edge Zone Width (m)	1.265	1.265	0.000	0.000	
Reduction Factor	0.600	1.000	1.000	1.000	
Factored Main Zone Coefficient	-0.347	-0.386	-0.579	-0.482	
Factored Edge Zone Coefficient	-1.042	-0.868	-0.579	-0.482	Ŧ

Fig 1.3 Left roof slope external surface coefficients

Wind Blowing From	Left	Right	Near	Far	1 -	
Right Roof/Rafter						
Size Effect Factor Ca	0.936	0.936	0.936	0.936		
Basic Main Zone Coefficient	-0.400	-0.600	-0.600	-0.500		
Basic Edge Zone Coefficient	-0.900	-1.800	-0.600	-0.500		
Edge Zone Width (m)	1.265	1.265	0.000	0.000		
Reduction Factor	1.000	0.600	1.000	1.000	-	
Factored Main Zone Coefficient	-0.386	-0.347	-0.579	-0.482		
Factored Edge Zone Coefficient	-0.868	-1.042	-0.579	-0.482	-	

Fig 1.4 Right roof slope external surface coefficients

With 10 % base partial fixity for deflection only, limiting height/horizontal deflection ratio 200, grade S275 steel and 7.5% span haunch lengths, the sections produced by autodesign are:

Rafters: 356 x 171 UKB 45 Columns: 406 x 178 UKB 60 Steel weight per frame: 1717 kg

These sections were selected from the UKB preferred list.

3.2 Duopitch portal frame building with left side open

The following text explains the modifications to be made for an open left side. The procedure is the same but 'handed' for an open right side but is given in full in section 3.3 to avoid cross referencing and interpretation. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2.

Wind direction θ	One	One open face		Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
Э0°ь	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	

Table 18 — Internal pressure coefficients $C_{\rm m}$ for open-sided huildings

Where two sets of values are given they should be treated as separate load cases.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension (a) for internal pressure is the diagonal dimension of the open face. In the present example if the whole left face is open the diagonal dimension is given with sufficient accuracy by:

> $Sqrt{36^2 + 5^2} =$ 36.3 m а



The corresponding size effect factor can be re	ad from	BS 639	9-2 fig 4 for a	site in co	untry >	2 km
from the sea:	Ca	=	0.85			
If only one bay is open	а	=	$Sqrt{6^{2} + 5^{2}}$	=	7.8	m
The corresponding size effect factor can be re	ad from	BS 639	9-2 fig 4 for a	site in co	ountry >	2 km
from the sea:	Ca	=	0.96			
For the purposes of the example let us assume	Са	=	0.90			

Therefore edit the value of Ca in fig 1.1 above from 0.739 to 0.90.

Internal surface coefficients - wind blowing from left

In BS 6399-2 Table 18, left wind equates to wind 0° blowing into the open longer face for which Cpi = 0.80. Therefore edit the default internal surface coefficient from +0.20 to + 0.80.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients - wind blowing from right

This direction equates to 180° in table 18 for which Cpi = -0.43. Therefore edit the default internal suction coefficient from -0.300 to -0.43.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients - wind blowing on near end

This direction equates to wind 90° in table 18 for which Cpi = + 0.67 or -0.46. These values actually correspond to wind directions slightly oblique to 90° . The positive pressure value occurs when the inclination directs the wind into the building whilst the negative suction value occurs when the inclination directs the wind away from the building. Therefore edit the default values +0.20 and -0.30 to +0.67 and -0.46 respectively.

Internal surface coefficients – wind blowing on far end

The internal coefficient values apply equally to far and near end wind.

After editing the internal surface coefficients should appear as shown in fig 5 below.

Wind Blowing From	Left	Right	Near	Far	*
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	
Inter	nal Surface Co	efficients			Ξ
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.800	0.200	0.670	0.670	
Factored Pressure Coefficient	0.742	0.186	0.622	0.622	
Basic Suction Coefficient	-0.300	-0.430	-0.460	-0.460	
Factored Suction Coefficient	-0.278	-0.399	-0.427	-0.427	Ŧ

Fig 2.1 Internal surface coefficients after editing for open left side.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open left side. The coefficients for the left side depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the left side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and, if necessary, justified.



In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the left column has cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for the equivalent closed sided building. In other circumstances the difference could be lesser or greater.

At the other extreme a left column may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column, the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying left external surface coefficients equal and opposite to the internal surface coefficients. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively two versions of the frame can be run:-

Case 2a: with the left column subject to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic coeff = 0.742/(1.031 x 0.963) = 0.747.

Wind Blowing From	Left	Right	Near	Far		
Left Wall/Column						
Size Effect Factor Ca	0.963	0.963	0.963	0.963	11	
Basic Pressure Coefficient	0.747	0.187	0.626	0.626	1	
Factored Pressure Coefficient	0.742	0.186	0.622	0.622		
	Right Wall/C	Column				
Size Effect Factor Ca	0.963	0.963	0.963	0.963		
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500		
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	1	

Fig 2.2 Edited external surface coefficients for case 2a.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2b: with the left column subject to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coeff = 0.399/(1.031 x 0.963) = 0.402.



Wind Blowing From	Left	Right	Near	Far	4		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.280	-0.402	-0.430	-0.430	1 1		
Factored Pressure Coefficient	-0.278	-0.399	-0.427	-0.427			
	Right Wall/Co	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	1		
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	-		

Fig 2.3 shows the edited external surface coefficients for case 2b.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 457 x 191 UKB 74 Steel weight per frame: 2089 kg

This represents a 22% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The internal pressure case 2a therefore governs the design

3.3 Duopitch portal frame building with right side open

The following text explains the modifications to be made for an open right side. The procedure is the same but `handed' for an open left side but is given in full in section 3.2 to avoid cross referencing. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2

Wind direction $ heta$	On	One open face		Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90°ь	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	

Table 18 — Internal pressure coefficients C_{pi} for open-sided buildings

two sets of values are given they should be treated as separate load cases.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole left face is open the diagonal dimension is given with sufficient accuracy by:

a =
$$Sqrt{36^2 + 5^2}$$
 = 36.3 m

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: 0.85 Ca = $Sqrt{6^{2} + 5^{2}}$ = If only one bay is open = 7.8 а m

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: 0.96 Ca =

0.90 For the purposes of the example let us assume Ca =

Therefore edit the value of Ca in fig 1.1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left



This direction equates to 180° in table 18 for which Cpi = -0.43. Therefore edit the default internal suction coefficient from -0.300 to -0.43.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients – wind blowing from right

In BS 6399-2 Table 18, right wind equates to wind 0° blowing into the open longer face for which Cpi = 0.80. Therefore edit the default internal pressure coefficient from +0.20 to + 0.80.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients - wind blowing on near end

This direction equates to wind 90° in table 18 for which Cpi = + 0.67 or -0.46. These values actually correspond to wind directions slightly oblique to 90° . The positive pressure value occurs when the inclination directs the wind into the building whilst the negative suction value occurs when the inclination directs the wind away from the building. Therefore edit the default values +0.20 and -0.30 to +0.67 and -0.46 respectively.

Internal surface coefficients – wind blowing on far end

The internal coefficient values apply equally to far and near end wind.

After editing the internal surface coefficients should appear as shown in fig 3.1 below.

Wind Blowing From	Left	Right	Near	Far	^
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	
Inter	nal Surface Co	efficients] ≡ [
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.200	0.800	0.670	0.670	
Factored Pressure Coefficient	0.186	0.742	0.622	0.622	1
Basic Suction Coefficient	-0.430	-0.300	-0.460	-0.460	1
Factored Suction Coefficient	-0.399	-0.278	-0.427	-0.427	Ŧ

Fig 3.1 Internal surface coefficients after editing for open right side.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open right side. The coefficients for the right side depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the right side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the right column has cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.



At the other extreme a right column may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column, the overall effect on the frame and the stability of the column may be critical. We will refer to this as case 2. In principle this case may be modelled by applying right side external surface coefficients equal and opposite to the internal coefficients. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients for the cases where the wind code provides alternative + and – coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively two versions of the frame can be run:-

Case 2a: with the right column subject to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coeff = 0.742/(1.031 x 0.963) = 0.747.

Wind Blowing From	Left	Right	Near	Far	•			
	Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=			
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500				
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497	1			
	Right Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963				
Basic Pressure Coefficient	0.187	0.747	0.626	0.626				
Factored Pressure Coefficient	0.186	0.742	0.622	0.622	-			

Fig 3.2 Edited external surface coefficients for case 2a.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2b with the right column subject to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coeff = -0.399/(1.031 x 0.963) = -0.402.



Wind Blowing From	Left	Right	Near	Far	14		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500			
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497			
	Right Wall/C	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.280	-0.402	-0.430	-0.430			
Factored Pressure Coefficient	-0.278	-0.399	-0.427	-0.427	1.		

Fig 3.3 Edited external surface coefficients for case 2b

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 457 x 191 UKB 74 Steel weight per frame: 2089 kg

This represents a 22% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The internal pressure case 2a therefore governs the design

3.4 Duopitch portal building with near side open

The following text explains the modifications to be made for an open near side. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2

Wind direction θ	One open face		Two adjacent	Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90° ^b	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
^a Values given should be	e applied to underside o	f roof only. For the single	wall, use pressure coefficient	s for walls given in Table 5	

Table 18 — Internal pressure coefficients $C_{\rm pi}$ for open-sided buildings

^b Where two sets of values are given they should be treated as separate load cases.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole near face is open the diagonal dimension is given with sufficient accuracy by:

	а	=	$Sqrt{20^2 + 5^2}$	=	20.6	m
The corresponding size effect factor can be refrom the sea:	ead from Ca	BS 639 =	99-2 fig 4 for a 0.89	site in	country	>2 km
If only a quarter of the side is open	а	=	$Sqrt{5^{2} + 5^{2}}$	=	7.1	m
The corresponding size effect factor can be refrom the sea:	ead from Ca	BS 639 =	99-2 fig 4 for a 0.98	site in	country	>2 km
For the purposes of the example let us assume	Ca	=	0.90			

Therefore edit the value of Ca in fig 1.1 above from 0.739 to 0.90.



Internal surface coefficients – wind blowing from left

This direction equates to 90° in table 18 for which Cpi = -0.60 and +0.52. These values actually correspond to wind directions slightly oblique to 90° . The positive pressure value occurs when the inclination directs the wind into the building whilst the negative suction value occurs when the inclination directs the wind away from the building. Therefore edit the default internal coefficients from -0.300 and +0.20 to -0.60 and +0.52.

Internal surface coefficients – wind blowing from right

This direction equates to 90° in table 18 for which Cpi = -0.60 and +0.52. The positive pressure value occurs when the inclination directs the wind into the building whilst the negative suction value occurs when the inclination directs the wind away from the building. Therefore edit the default internal coefficients from -0.300 and +0.20 to -0.60 and +0.52.

Internal surface coefficients - wind blowing on near end

This direction equates to 0° in table 18 for which Cpi = +0.85. There is no corresponding suction value so leave the default -0.30 unchanged.

Internal surface coefficients – wind blowing on far end

This direction equates to 180° in table 18 for which Cpi = -0.39 There is no corresponding pressure value so leave the default +0.20 unchanged.

Left	Right	Near	Far	^
0.751	0.751	0.751	0.751	
1.031	1.031	1.031	1.031	1
nal Surface Co	efficients			Ξ
0.900	0.900	0.900	0.900	1
0.520	0.520	0.850	0.200	1
0.483	0.483	0.789	0.186	1
-0.600	-0.600	-0.300	-0.390	1
-0.557	-0.557	-0.278	-0.362	-
	Left 0.751 1.031 nal Surface Co 0.900 0.520 0.483 -0.600 -0.557	Left Right 0.751 0.751 1.031 1.031 nal Surface Coefficients 0.900 0.900 0.900 0.520 0.520 0.483 0.483 -0.600 -0.600 -0.557 -0.557	Left Right Near 0.751 0.751 0.751 1.031 1.031 1.031 nal Surface Coefficients 0.900 0.900 0.520 0.520 0.850 0.483 0.483 0.789 -0.600 -0.600 -0.300 -0.557 -0.557 -0.278	Left Right Near Far 0.751 0.751 0.751 0.751 1.031 1.031 1.031 1.031 nal Surface Coefficients 0.900 0.900 0.900 0.520 0.520 0.850 0.200 0.483 0.483 0.789 0.186 -0.600 -0.600 -0.300 -0.390

After editing, the internal surface coefficients should appear as shown in fig 4.1 below.

Fig 4.1 Internal surface coefficients after editing for open near side.

External surface coefficients

The external surface coefficients for main frames are unchanged from the default values for a building with closed sides.

Autodesign produces the following sections for this example:

Rafters: 356 x 171 UKB 51 Columns: 406 x 178 UKB 60 Steel weight per frame: 1854 kg

This represents a 8% increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.

3.5 Duopitch portal building with far side open

The following text explains the modifications to be made for an open far side. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2



Wind direction θ	On	One open face		Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90 ^{°ь}	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
 ^a Values given should b ^b Where two sets of values 	e applied to underside o les are given they shoul	f roof only. For the single d be treated as separate lo	wall, use pressure coefficient oad cases.	s for walls given in Table 5.	

Table 18 — Internal pressure coefficients C_{pi} for open-sided buildings

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole near face is open the diagonal dimension is given with sufficient accuracy by:

	а	=	$Sqrt{20^{2} + 5^{2}}$	=	20.6	m
The corresponding size effect factor can be refrom the sea:	ad from Ca	BS 639 =	9-2 fig 4 for a : 0.89	site in co	ountry >	∙2 km
If only a quarter of the side is open	а	=	$Sqrt{52 + 52}$	=	7.1	m
The corresponding size effect factor can be refrom the sea:	ad from Ca	BS 639 =	9-2 fig 4 for a : 0.98	site in co	ountry >	∙2 km
For the purposes of the example let us assume	Ca	=	0.90			

Therefore edit the value of Ca in fig 1.1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left

This direction equates to 90° in table 18 for which Cpi = -0.60 and +0.52. These values actually correspond to wind directions slightly oblique to 90° . The positive pressure value occurs when the inclination directs the wind into the building whilst the negative suction value occurs when the inclination directs the wind away from the building.Therefore edit the default internal coefficients from -0.300 and +0.20 to -0.60 and +0.52.

Internal surface coefficients – wind blowing from right

This direction equates to 90° in table 18 for which Cpi = -0.60 and +0.52. The positive pressure value occurs when the inclination directs the wind into the building whilst the negative suction value occurs when the inclination directs the wind away from the building. Therefore edit the default internal coefficients from -0.300 and +0.20 to -0.60 and +0.52.

Internal surface coefficients - wind blowing on near end

This direction equates to 180° in table 18 for which Cpi = -0.39 There is no corresponding pressure value so leave the default +0.20 unchanged.

Internal surface coefficients - wind blowing on far end

This direction equates to 0° in table 18 for which Cpi = +0.85. There is no corresponding suction value so leave the default -0.30 unchanged.

After editing the internal surface coefficients should appear as shown in fig 5.1 below.



Wind Blowing From	Left	Right	Near	Far	
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1
Inter	nal Surface Co	efficients			Ξ
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.520	0.520	0.200	0.850	
Factored Pressure Coefficient	0.483	0.483	0.186	0.789	1
Basic Suction Coefficient	-0.600	-0.600	-0.390	-0.300	1
Factored Suction Coefficient	-0.557	-0.557	-0.362	-0.278	Ŧ

Fig 5.1 Internal surface coefficients after editing for open far side.

External surface coefficients

The external surface coefficients for main frames are unchanged from the default values for a building with closed sides.

Autodesign produces the following sections for this example:

Autodesign produces the following sections for this example:

Rafters: 356 x 171 UKB 51 Columns: 406 x 178 UKB 60 Steel weight per frame: 1854 kg

This represents a 8% increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.

3.6 Duopitch portal building with near and left sides open

The following text explains the modifications to be made for two adjacent sides open. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2:

Wind direction θ	One open face		Two adjacent	Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90°ь	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
^a Values given should b	e applied to underside o	f roof only. For the single	wall, use pressure coefficient	s for walls given in Table 5	

Table 18 — Internal pressure coefficients $C_{\rm pi}$ for open-sided buildings

a Values given should be applied to underside of roof only. For the single wall, use pressure coefficients for walls given in Table 5.
b Where two sets of values are given they should be treated as separate load cases.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole left face is open the diagonal dimension is given with sufficient accuracy by:

a =
$$Sqrt{36^2 + 5^2}$$
 = 36.3 m

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: Ca = 0.85

If only one bay is open a = $Sqrt\{6^2 + 5^2\}$ = 7.8

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: Ca = 0.96



m

For the purposes of the example let us assume Ca = 0.90

Therefore edit the value of Ca in fig 1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left

In BS 6399-2 Table 18, left wind equates to wind 0° blowing into the open side face for which Cpi = 0.77. Therefore edit the default internal pressure coefficient from +0.20 to + 0.77.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients - wind blowing from right

This direction equates to 180° in table 18 for which Cpi = -0.60. Therefore edit the default internal suction coefficient from -0.300 to -0.60.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients - wind blowing on near end

This direction equates to wind 90° in table 18 for which Cpi = + 0.77 or -0.57. The positive coefficient corresponds to wind blowing into the open near end. Therefore edit the default values +0.20 and -0.30 to +0.77 and -0.30 respectively.

Internal surface coefficients - wind blowing on far end

This direction equates to wind 90° in table 18 for which Cpi = + 0.77 or -0.57. The negative coefficient corresponds to wind blowing onto the closed far end. Therefore edit the default values +0.20 and -0.30 to +0.20 and -0.57 respectively.

Wind Blowing From	Left	Right	Near	Far	^
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	
Inter	nal Surface Co	efficients			Ξ
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.770	0.200	0.770	0.200	
Factored Pressure Coefficient	0.715	0.186	0.715	0.186	1
Basic Suction Coefficient	-0.300	-0.600	-0.300	-0.570	
Factored Suction Coefficient	-0.278	-0.557	-0.278	-0.529	Ŧ

After editing the internal surface coefficients should appear as shown in fig 6.1 below.

Fig 6.1 Internal surface coefficients after editing for open left and near sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open left side. The coefficients for the left side depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the left side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the left column has cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:



Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This solution is the same as left or right side open only and represents a 5% weight increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.

At the other extreme a left column may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column, the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying left external surface coefficients equal and opposite to the internal surface coefficients. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients which will also cater for the cases where the wind code provides alternative + and – coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively two versions of the frame can be run:-

• Case 2a: with the left column subject to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic coeff = 0.715/(1.031 x 0.963) = 0.720.

Wind Blowing From	Left	Right	Near	Far	-
	Left Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	0.720	0.187	0.720	0.187	
Factored Pressure Coefficient	0.715	0.186	0.715	0.186	
	Right Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	Ŧ

Fig 6.2 Edited external surface coefficients for case 6a

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 60 Columns: 533 x 210 UKB 82 Steel weight per frame: 2319 kg

This represents a 35% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2b with the left column subject to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coefficient = -0.557/(1.031 x 0.963) = 0.561.



Wind Blowing From	Left	Right	Near	Far	-
	Left Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	-0.280	-0.561	-0.280	-0.574	
Factored Pressure Coefficient	-0.278	-0.557	-0.278	-0.570	
	Right Wall/Co	olumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	-

Fig 6.3 Edited external surface coefficients for case 6b

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The internal pressure case 2a therefore governs the design

3.7 Duopitch portal building with near and right sides open

The following text explains the modifications to be made for two adjacent sides open. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2:

Wind direction θ	On	e open face	Two adjacent	Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90°ь	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
a Values given should be	e applied to underside o	froof only For the single .		E 11 1 1 1 1 1 1 1	

Table 18 — Internal pressure coefficients C_{pi} for open-sided buildings

a Values given should be applied to underside of roof only. For the single wall, use pressure coefficients for walls given in Table 5.
b Where two sets of values are given they should be treated as separate load cases.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole left face is open the diagonal dimension is given with sufficient accuracy by:

	а	=	Sqrt{36 ² + 5 ² }	=	36.3	m
The corresponding size effect factor can be re from the sea:	ad from Ca	BS 639 =	9-2 fig 4 for a 0.85	site in	country	>2 km
If only one bay is open	а	=	$Sqrt{6^{2} + 5^{2}}$	=	7.8	m
The corresponding size effect factor can be re from the sea:	ad from Ca	BS 639 =	9-2 fig 4 for a 0.96	site in	country	>2 km
For the purposes of the example let us assume	Са	=	0.90			
Therefore edit the value of Ca in fig 1 above fro	om 0.739	9 to 0.90).			

Internal surface coefficients – wind blowing from left



This direction equates to 180° in table 18 for which Cpi = -0.60. Therefore edit the default internal suction coefficient from -0.300 to -0.60.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients - wind blowing from right

In BS 6399-2 Table 18, right wind equates to wind 0° blowing into the open side face for which Cpi = 0.77. Therefore edit the default internal pressure coefficient from +0.20 to + 0.77.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients - wind blowing on near end

This direction equates to wind 90° in table 18 for which Cpi = + 0.77 or -0.57. The positive coefficient corresponds to wind blowing into the open near end. Therefore edit the default values +0.20 and -0.30 to +0.77 and -0.30 respectively.

Internal surface coefficients – wind blowing on far end

This direction equates to wind 90° in table 18 for which Cpi = + 0.77 or -0.57. The negative coefficient corresponds to wind blowing onto the closed far end. Therefore edit the default values +0.20 and -0.30 to +0.20 and -0.57 respectively.

Wind Blowing From	Left	Right	Near	Far	-
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1
Inter	nal Surface Co	efficients			Ξ
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.200	0.770	0.770	0.200	
Factored Pressure Coefficient	0.186	0.715	0.715	0.186	1
Basic Suction Coefficient	-0.600	-0.300	-0.300	-0.570	1
Factored Suction Coefficient	-0.557	-0.278	-0.278	-0.529	Ŧ

After editing the internal surface coefficients should appear as shown in fig 7.1 below.

Fig 7.1 Internal surface coefficients after editing for open near and right sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open right side. The coefficients for the right side depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the right side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the right column has cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg



This solution is the same as left or right side open only and represents a 5% weight increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.

At the other extreme a right column may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column, the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying right side external surface coefficients equal and opposite to the internal pressure coefficients. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients which will also cater for the cases where the wind code provides alternative + and – coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively two versions of the frame can be run:-

Case 2a: with the right column subject to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coeff = 0.715/(1.031 x 0.963) = 0.720.

Wind Blowing From	Left	Right	Near	Far				
Left Wall/Column								
Size Effect Factor Ca	0.963	0.963	0.963	0.963				
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500				
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497				
	Right Wall/Co	olumn						
Size Effect Factor Ca	0.963	0.963	0.963	0.963				
Basic Pressure Coefficient	0.720	0.187	0.720	0.187				
Factored Pressure Coefficient	0.715	0.186	0.715	0.186				

Fig 7.2 Edited external surface coefficients for case 2a

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 60 Columns: 533 x 210 UKB 82 Steel weight per frame: 2319 kg

This represents a 35% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2b with the right column subject to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coefficient = -0.557/(1.031 x 0.963) = 0.561.



Wind Blowing From	Left	Right	Near	Far	1	
Size Effect Factor Ca	0.963	0.963	0.963	0.963	16	
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500	1 =	
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497	14	
	Right Wall/C	olumn				
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1	
Basic Pressure Coefficient	-0.280	-0.561	-0.280	-0.561	1	
Factored Pressure Coefficient	-0.278	-0.557	-0.278	-0.557	1	
Left Roof/Rafter						

Fig 7.3 Edited external surface coefficients for case 2b

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 457 x 191 UKB 67 Steel weight per frame: 2007 kg

This represents a 17% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The internal pressure case 2a therefore governs the design

3.8 Duopitch portal building with far and left sides open

The following text explains the modifications to be made for two adjacent sides open. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2:

Wind direction θ	On	e open face	Two adjacent	Three open faces ^a	
	Shorter Longer		open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90° ^b	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
 Values given should be Where two sets of values 	e applied to underside o les are given they shoul	f roof only. For the single v d be treated as separate lo	wall, use pressure coefficient	s for walls given in Table 5.	

Table 18 — Internal pressure coefficients $C_{\rm pi}$ for open-sided buildings

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole left face is open the diagonal dimension is given with sufficient accuracy by:

a =
$$Sqrt{36^2 + 5^2}$$
 = 36.3 m

 $Sqrt\{6^2 + 5^2\}$

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: Ca = 0.85

а

=

If only one bay is open

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: Ca = 0.96

For the purposes of the example let us assume Ca = 0.90

Therefore edit the value of Ca in fig 1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left



=

7.8

m

In BS 6399-2 Table 18, left wind equates to wind 0° blowing into the open side face for which Cpi = 0.77. Therefore edit the default internal pressure coefficient from +0.20 to + 0.77.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients – wind blowing from right

This direction equates to 180° in table 18 for which Cpi = -0.60. Therefore edit the default internal suction coefficient from -0.300 to -0.60.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients - wind blowing on near end

This direction equates to wind 90° in table 18 for which Cpi = + 0.77 or -0.57. The negative coefficient corresponds to wind blowing onto the closed near end. Therefore edit the default values +0.20 and -0.30 to +0.20 and -0.57 respectively.

Internal surface coefficients - wind blowing on far end

This direction equates to wind 90° in table 18 for which Cpi = + 0.77 or -0.57. The positive coefficient corresponds to wind blowing into the open far end. Therefore edit the default values +0.20 and -0.30 to +0.77 and -0.30 respectively.

Wind Blowing From	Left	Right	Near	Far	-
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1
Inter	nal Surface Co	efficients			E
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.770	0.200	0.200	0.770	
Factored Pressure Coefficient	0.715	0.186	0.186	0.715	1
Basic Suction Coefficient	-0.300	-0.600	-0.570	-0.300	1
Factored Suction Coefficient	-0.278	-0.557	-0.529	-0.278	-

After editing the internal surface coefficients should appear as shown in fig 8.1 below.

Fig 8.1 Internal surface coefficients after editing for open left and far sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open left side. The coefficients for the left side depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the left side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the left column has cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg



This solution is the same as left or right side open only and represents a 5% weight increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.

At the other extreme a left column may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column, the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying left external surface coefficients equal and opposite to the internal surface coefficients. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients which will also cater for the cases where the wind code provides alternative + and – coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively two versions of the frame can be run:-

Case 2a: with the left column subject to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic coeff = 0.715/(1.031 x 0.963) = 0.720.

Wind Blowing From	Left	Right	Near	Far			
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	0.720	0.187	0.187	0.720			
Factored Pressure Coefficient	0.715	0.186	0.186	0.715			
	Right Wall/Co	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500			
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497			

Fig 8.2 Edited external surface coefficients for case 2a

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 457 x 191 UKB 74 Steel weight per frame: 2089 kg

This represents a 22% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2b with the left column subject to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coefficient = -0.557/(1.031 x 0.963) = 0.561.



Wind Blowing From	Left	Right	Near	Far	-			
	Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=			
Basic Pressure Coefficient	-0.280	-0.561	-0.533	-0.280				
Factored Pressure Coefficient	-0.278	-0.557	-0.530	-0.278				
	Right Wall/Co	olumn						
Size Effect Factor Ca	0.963	0.963	0.963	0.963				
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500				
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	-			

Fig 8.3 Edited external surface coefficients for case 2b

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The internal suction case 2b therefore governs the design

3.9 Duopitch portal building with far and right sides open

The following text explains the modifications to be made for two adjacent sides open. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2:

Wind direction $ heta$	On	e open face	Two adjacent	Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90° ^b	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
 ^a Values given should be ^b Where two sets of values 	e applied to underside o	f roof only. For the single	wall, use pressure coefficient	s for walls given in Table 5.	

Table 18 — Internal pressure coefficients $C_{\rm pi}$ for open-sided buildings

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole right face is open the diagonal dimension is given with sufficient accuracy by:

a =
$$Sqrt{36^2 + 5^2}$$
 = 36.3 m

 $Sqrt{6^{2} + 5^{2}}$

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: Ca = 0.85

=

If only one bay is open

= 7.8 m

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: Ca = 0.96

а

For the purposes of the example let us assume Ca = 0.90

Therefore edit the value of Ca in fig 1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left



This direction equates to 180° in table 18 for which Cpi = -0.60. Therefore edit the default internal suction coefficient from -0.300 to -0.60.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients - wind blowing from right

In BS 6399-2 Table 18, right wind equates to wind 0° blowing into the open side face for which Cpi = 0.77. Therefore edit the default internal pressure coefficient from +0.20 to + 0.77.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients - wind blowing on near end

This direction equates to wind 90° in table 18 for which Cpi = + 0.77 or -0.57. The negative coefficient corresponds to wind blowing onto the closed near end. Therefore edit the default values +0.20 and -0.30 to +0.20 and -0.57 respectively.

Internal surface coefficients - wind blowing on far end

This direction equates to wind 90° in table 18 for which Cpi = + 0.77 or -0.57. The positive coefficient corresponds to wind blowing into the open far end. Therefore edit the default values +0.20 and -0.30 to +0.77 and -0.30 respectively.

Wind Blowing From	Left	Right	Near	Far	-
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1
Inter	nal Surface Co	efficients			E
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.200	0.770	0.200	0.770	
Factored Pressure Coefficient	0.186	0.715	0.186	0.715	
Basic Suction Coefficient	-0.600	-0.300	-0.570	-0.300	
Factored Suction Coefficient	-0.557	-0.278	-0.529	-0.278	Ŧ

After editing the internal surface coefficients should appear as shown in fig 9.1 below.

Fig 9.1 Internal surface coefficients after editing for open far and right sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open right side. The coefficients for the right side depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the right side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the right column has cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg



This solution is the same as left or right side open only and represents a 5% weight increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.

At the other extreme a right column may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column, the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying right side external surface coefficients equal and opposite to the internal surface coefficients. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients which will also cater for the cases where the wind code provides alternative + and – coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively two versions of the frame can be run:-

Case 2a: with the right column subject to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coeff = 0.715/(1.031 x 0.963) = 0.720.

Left	Right	Near	Far	ľ			
Left Wall/Column							
0.963	0.963	0.963	0.963				
0.614	-0.500	-0.800	-0.500	1 1			
0.610	-0.497	-0.795	-0.497	1			
Right Wall/Co	lumn						
0.963	0.963	0.963	0.963				
0.187	0.720	0.187	0.720	1			
0.186	0.715	0.186	0.715	-			
	Left Wall/Col 0.963 0.614 0.610 Right Wall/Co 0.963 0.187 0.186	Left Right Left Wall/Column 0.963 0.963 0.963 0.614 -0.500 0.610 -0.497 Right Wall/Column 0.963 0.963 0.963 0.187 0.720 0.186 0.715	Left Right Near Left Wall/Column 0.963 0.963 0.963 0.614 -0.500 -0.800 0.610 0.610 -0.497 -0.795 0.963 Right Wall/Column 0.963 0.963 0.963 0.187 0.720 0.187 0.186	Left Right Near Far Left Wall/Column 0.963 0.963 0.963 0.963 0.614 -0.500 -0.800 -0.500 0.610 -0.497 -0.795 -0.497 Right Wall/Column 0.963 0.963 0.963 0.187 0.720 0.187 0.720 0.186 0.715 0.186 0.715			

Fig 9.2 Edited external surface coefficients for case 2a

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 457 x 191 UKB 74 Steel weight per frame: 2089 kg

This represents a 22% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2b with the right column subject to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coefficient = -0.557/(1.031 x 0.963) = 0.561.



Wind Blowing From	Left	Right	Near	Far	-			
	Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=			
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500				
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497				
	Right Wall/Co	olumn						
Size Effect Factor Ca	0.963	0.963	0.963	0.963				
Basic Pressure Coefficient	-0.561	-0.280	-0.280	-0.533				
Factored Pressure Coefficient	-0.557	-0.278	-0.278	-0.530	-			

Fig 9.3 Edited external surface coefficients for case 2b

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The internal suction case 2b therefore governs the design

3.10 Duopitch portal building with near and far sides open

The following text suggests modifications that might be made to the default wind coefficients to cater for open near and far sides. This condition is not covered by Table 18 of BS 6399-2. Section 2.6.3.2 briefly discusses the condition and refers to *The designer's guide to wind loading of building structures Part 2 sections 18.6.3 and 20.9.2.4*¹ for more detail. The latter reveals that experimental evidence is only available for overall force effects and attention is drawn to the case of wind blowing at 45 degrees to the main axes with the suggestion that an overall force coefficient of 2.2 could be divided between the clad sides. This could be modelled by changing the surface coefficients for the left and right walls under `left' wind to +1.1 and -1.1 respectively. Obviously the right wind coefficients would be -1.1 and +1.1. There is no information relating to internal surface pressures, however referring to Table 18 it seems unlikely that the range Cpi = -0.67 to +0.85 would be exceeded. The following text is based on the foregoing tentative interpretation and should be followed only at readers own discretion.

Wind direction $ heta$	One open face		Two adjacent	Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90°ь	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
 Values given should b Where two sets of values 	e applied to underside o ues are given they shoul	f roof only. For the single d be treated as separate lo	wall, use pressure coefficient	s for walls given in Table 5.	

Table 18 — Interna	l pressure	coefficients	$C_{\rm pi}$ for	open-sided	buildings
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Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole near face is open the diagonal dimension is given with sufficient accuracy by:

a = $Sqrt\{20^2 + 5^2\}$ = 20.6 m

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: Ca = 0.89



If only a quarter of the side is open	а	=	Sqrt{5 ² + 5 ² }	=	7.1	m
The corresponding size effect factor can be re	ead from	n BS	6399-2 fig 4 for a	site in	country	>2 km
from the sea:	Ca	=	0.98			
For the purposes of the example let us assume	Ca	=	0.90			

Therefore edit the value of Ca in fig 1.1 above from 0.739 to 0.90.

Internal surface coefficients

From the above discussion it is suggested that the internal pressure and suction coefficients are unlikely to be worse than + 0.85 and -0.67. These values actually correspond to wind directions oblique to the X (left – right) axis. The positive pressure value occurs when the inclination directs the wind into the building whilst the negative suction value occurs when the inclination directs the wind away from the building. This will happen at different frames. Therefore edit the default internal coefficients from -0.300 and +0.20 to -0.65 and +0.85.

After editing, the internal surface coefficients should appear as shown in fig 10.1 below.

Wind Blowing From	Left	Right	Near	Far	^
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	
Inter	nal Surface Co	efficients			Ξ
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.850	0.850	0.850	0.850	
Factored Pressure Coefficient	0.789	0.789	0.789	0.789	
Basic Suction Coefficient	-0.670	-0.670	-0.670	-0.670	
Factored Suction Coefficient	-0.622	-0.622	-0.622	-0.622	Ŧ

Fig 10.1 Internal surface coefficients after editing for open near and far sides.

External surface coefficients

The external surface coefficients for main frames are only changed from the default values for a building with closed sides in respect of the left and right walls with wind blowing from left or right. As explained above the changes in fact model wind acting obliquely. After editing the external surface coefficients should appear as shown in fig 10.2 below.

Wind Blowing From	Left	Right	Near	Far	
	Left Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	1.100	-1.100	-0.800	-0.500	
Factored Pressure Coefficient	1.093	-1.093	-0.795	-0.497	
	Right Wall/Co	olumn	·		
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	-1.100	1.100	-0.800	-0.500	
Factored Pressure Coefficient	-1.093	1.093	-0.795	-0.497	-

Fig 10.2 External surface coefficients after editing for open near and far sides.

Note that the external coeficients for the roof surfaces are unchanged from the default values for a closed sided building.

Autodesign produces the following sections for this example:

Rafters: 406 x 178 UKB 60 Columns: 533 x 210 UKB 82 Steel weight per frame: 2319 kg

This represents a 35 % increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.



3.11 Duopitch portal building with left and right sides open

The following text suggests modifications that might be made to the default wind coefficients to cater for open left and right sides. This condition is not covered by Table 18 of BS 6399-2. Section 2.6.3.2 briefly discusses the condition and refers to *The designer's guide to wind loading of building structures Part 2 by NJ Cook sections 18.6.3 and 20.9.2.4*¹ for more detail. The latter reveals that experimental evidence is only available for overall force effects and attention is drawn to the case of wind blowing at 45 degrees to the main axes with the suggestion that an overall force coefficient of 2.2 could be divided between the clad sides. This could be modelled by changing the surface coefficients for the clad near and far end walls under `left' wind to +1.1 and -1.1 respectively. Obviously the right wind coefficients would be -1.1 and +1.1. There is no information relating to internal surface pressures. However referring to Table 18 it seems unlikely that the range Cpi = -0.67 to +0.85 would be exceeded. The following text is based on the foregoing tentative interpretation and should be followed only at readers own discretion.

Wind direction $ heta$	One	e open face	Two adjacent	Three open faces ^a
	Shorter	Longer	open faces	
0°	+0.85	+0.80	+0.77	+0.60
90° ^b	-0.60	-0.46	-0.57	-0.63
	+0.52	+0.67	+0.77	+0.40
180°	-0.39	-0.43	-0.60	-0.56

Table 18 —	Internal	pressure	coefficients	C_{pi}	for	open-sided	buildings
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Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole left/right face is open the diagonal dimension is given with sufficient accuracy by:

	а	=	$Sqrt{36^{2} + 5^{2}}$	=	36.3	m
The corresponding size effect factor can be refrom the sea:	ead from Ca	BS 639 =	9-2 fig 4 for a 0.85	site in	country	>2 km
If only one bay is open	а	=	$Sqrt{6^{2} + 5^{2}}$	=	7.8	m
The corresponding size effect factor can be refrom the sea:	ead from Ca	BS 639 =	9-2 fig 4 for a 0.96	site in	country	>2 km
For the purposes of the example let us assume	Ca	=	0.90			

Therefore edit the value of Ca in fig 1.1 above from 0.739 to 0.90.

Internal surface coefficients

From the above discussion it is suggested that the internal pressure and suction coefficients are unlikely to be worse than + 0.85 and -0.67. These values actually correspond to wind directions oblique to the X (left – right) axis. The positive pressure value occurs when the inclination directs the wind into the building whilst the negative suction value occurs when the inclination directs the wind away from the building. This will happen at different frames. Therefore edit the default internal coefficients from -0.300 and +0.20 to -0.67 and +0.85.

After editing, the internal surface coefficients should appear as shown in fig 11.1 below.



Wind Blowing From	Left	Right	Near	Far		
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751		
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1	
Internal Surface Coefficients						
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900		
Basic Pressure Coefficient	0.850	0.850	0.850	0.850		
Factored Pressure Coefficient	0.789	0.789	0.789	0.789	1	
Basic Suction Coefficient	-0.670	-0.670	-0.670	-0.670	1	
Factored Suction Coefficient	-0.622	-0.622	-0.622	-0.622	Ŧ	

Fig 11.1 Internal surface coefficients after editing for open left and right sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open left and right sides. The coefficients for the left and right sides depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the left or right side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the columns have cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This solution is 5% heavier than the design for the equivalent closed sided building as given in section 3.1. In other circumstances there may be differences. At the other extreme a left or right column (or both) may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column(s), the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying external surface coefficients equal and opposite to the internal surface coefficients on the relevant columns. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively several versions of the frame can be run:-

• Case 2a: Left column without cladding. Right column with cladding. Internal pressure.

The left column is subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.789/(1.031 \times 0.963) = 0.795$.



Wind Blowing From	Left	Right	Near	Far	
	Left Wall/C	olumn	-		
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	0.795	0.795	0.795	0.795	
Factored Pressure Coefficient	0.790	0.790	0.790	0.790	
	Right Wall/	Column			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	

Fig 11.2 Edited external surface coefficients for case 2a.

Autodesign produces the following sections for this case:

Rafters: 457 x 191 UKB 67 Columns: 457 x 191 UKB 74 Steel weight per frame: 2387 kg

This represents a 39% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2b: Left column without cladding. Right column with cladding. Internal suction.

The left column is subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.622/(1.031 \times 0.963) = -0.626$.

Wind Blowing From	Left	Right	Near	Far	1
	Left Wall/Col	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	-0.626	-0.626	-0.626	-0.626	
Factored Pressure Coefficient	-0.622	-0.622	-0.622	-0.622	
	Right Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	-

Fig 11.3 shows the edited external surface coefficients for case 2b.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 60 Columns: 533 x 210 UKB 82 Steel weight per frame: 2319 kg

This represents a 35% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2b also passes with the sections selected for case 2a

• Case 2c: Left column with cladding. Right column without cladding. Internal pressure.

The right column is subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.789/(1.031 \times 0.963) = 0.795$.



Wind Blowing From	Left	Right	Near	Far	-		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=		
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500			
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497			
	Right Wall/Co	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	0.795	0.795	0.795	0.795			
Factored Pressure Coefficient	0.790	0.790	0.790	0.790	-		

Fig 11.4 Edited external surface coefficients for case 2c.

Autodesign produces the following sections for this case:

Rafters: 457 x 191 UKB 67 Columns: 457 x 191 UKB 74 Steel weight per frame: 2387 kg

This represents a 39% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2d: Left column with cladding. Right column without cladding. Internal suction.

The right column is subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.622/(1.031 \times 0.963) = -0.626$.

Wind Blowing From	Left	Right	Near	Far	
	Left Wall/Col	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500	
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497	
	Right Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	-0.626	-0.626	-0.626	-0.626	
Factored Pressure Coefficient	-0.622	-0.622	-0.622	-0.622	Ŧ

Fig 11.5 shows the edited external surface coefficients for case 2d.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 60 Columns: 533 x 210 UKB 82 Steel weight per frame: 2319 kg

This represents a 35% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2d also passes with the sections selected for case 2c

Case 2e: Left column without cladding. Right column without cladding. Internal pressure.

The left and right columns are subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.789/(1.031 \times 0.963) = 0.795$.



Wind Blowing From	Left	Right	Near	Far	1 ^
	Left Wall/Co	lumn	-		1
Size Effect Factor Ca	0.963	0.963	0.963	0.963	115
Basic Pressure Coefficient	0.795	0.795	0.795	0.795	
Factored Pressure Coefficient	0.790	0.790	0.790	0.790	1
	Right Wall/C	olumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	0.795	0.795	0.795	0.795	1
Factored Pressure Coefficient	0.790	0.790	0.790	0.790	-

Fig 11.6 Edited external surface coefficients for case 2e.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The column sizes were increased for member stability.

• Case 2f: Left column without cladding. Right column without cladding. Internal suction.

The left and right columns are subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.622/(1.031 \times 0.963) = -0.626$.

Wind Blowing From	Left	Right	Near	Far	-
	Left Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	-0.626	-0.626	-0.626	-0.626	
Factored Pressure Coefficient	-0.622	-0.622	-0.622	-0.622	
	Right Wall/Co	olumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	-0.626	-0.626	-0.626	-0.626	
Factored Pressure Coefficient	-0.622	-0.622	-0.622	-0.622	-

Fig 11.7 Edited external surface coefficients for case 2f.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

For this particular frame configuration the design outcomes may be summarised as follows:-

	Rafters	Columns	Weight				
Left and right columns clad	356x171UKB45	406x178UKB60	1717	kg	100%		
Left unclad right clad	457x191UKB67	457x191UKB74	2387	kg	139%		
Left clad right unclad	457x191UKB67	457x191UKB74	2387	kg	139%		
Both sides unclad	356x171UKB45	457x191UKB67	1798	kg	105%		
Clearly the unsymmetrically cla	Clearly the unsymmetrically clad case is critical.						



3.12 Duopitch portal building with near, far and left sides open

The following text explains the modifications to be made for three adjacent sides open. The procedure is the same but `handed' for an open near, far and right sides but is given in full in section 3.13 to avoid cross referencing and interpretation. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2:

Wind direction θ	On	e open face	Two adjacent	Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90 ^{°ь}	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
 ^a Values given should b ^b Where two sets of values 	e applied to underside o les are given they shoul	f roof only. For the single d be treated as separate lo	wall, use pressure coefficient ad cases.	s for walls given in Table 5.	

Table 18 — I	nternal pressure	coefficients C_{pi} f	for open-sided	buildings
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Attention is drawn to note (a) to the table which applies when the left side is completely open. The implication here is that different internal surface coefficients are applicable to the roof and walls. This does not seem entirely logical and cannot be accommodated in the present version of SMART Portal. However the difference between applying the relevant table 5 and table 18 coefficients to the single wall is marginal and of the same order as the uncertainties implicit in the guidance. Therefore it is proposed to ignore note (a) in the interests of simplicity and practical use of the software.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole left face is open the diagonal dimension is given with sufficient accuracy by:

	а	=	$Sqrt{36^{2} + 5^{2}}$	=	36.3	m
The corresponding size effect factor can be re from the sea:	ad from Ca	BS 639 =	9-2 fig 4 for a 0.85	site in	country	>2 km
If only one bay is open	а	=	$Sqrt{6^{2} + 5^{2}}$	=	7.8	m
The corresponding size effect factor can be re from the sea:	ad from Ca	BS 639 =	9-2 fig 4 for a 0.96	site in	country	>2 km
For the purposes of the example let us assume	Са	=	0.90			

Therefore edit the value of Ca in fig 1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left

In BS 6399-2 Table 18, left wind equates to wind 0° blowing into the open longer face for which Cpi = 0.60. Therefore edit the default internal pressure coefficient from +0.20 to + 0.60.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients – wind blowing from right



This direction equates to 180° in table 18 for which Cpi = -0.56. Therefore edit the default internal suction coefficient from -0.300 to -0.56.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients - wind blowing on near end

This direction equates to wind 90° in table 18 for which Cpi = + 0.40 or -0.63. The positive coefficient corresponds to wind blowing into the building at a skew angle so as to attack the inside face of the right wall. The negative coefficient corresponds to wind blowing onto the building at a skew angle so as to attack the outside face of the right wall. Therefore edit the default values +0.20 and -0.30 to +0.40 and -0.63 respectively.

Internal surface coefficients - wind blowing on far end

This direction equates to wind 90° in table 18 for which Cpi = + 0.40 or -0.63. The positive coefficient corresponds to wind blowing into the building at a skew angle so as to attack the inside face of the right wall. The negative coefficient corresponds to wind blowing onto the building at a skew angle so as to attack the outside face of the right wall. Therefore edit the default values +0.20 and -0.30 to +0.40 and -0.63 respectively.

Wind Blowing From	Left	Right	Near	Far	^
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1
Inter	nal Surface Co	efficients			
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.600	0.200	0.400	0.400	
Factored Pressure Coefficient	0.557	0.186	0.371	0.371	1
Basic Suction Coefficient	-0.300	-0.560	-0.630	-0.630]
Factored Suction Coefficient	-0.278	-0.520	-0.585	-0.585	-

After editing the internal surface coefficients should appear as shown in fig 11 below.

Fig 12.1 Internal surface coefficients after editing for open left, near and far sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open left side. The coefficients for the left side depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the left side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the left column has cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 51 Columns: 406 x 178 UKB 60 Steel weight per frame: 1854 kg

This solution represents an 8% increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.

At the other extreme a left column may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column, the overall



effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying left external surface coefficients equal and opposite to the internal surface coefficients. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients which will also cater for the cases where the wind code provides alternative + and – coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively two versions of the frame can be run:-

• Case 2a: with the left column subject to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic coeff = -0.557/(1.031 x 0.963) = 0.561.

Wind Blowing From	Left	Right	Near	Far	Π		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1 *		
Basic Pressure Coefficient	0.561	0.187	0.373	0.373	1 1		
Factored Pressure Coefficient	0.557	0.186	0.371	0.371	1		
	Right Wall/C	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	1		
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	,		

Fig 12.2 Edited external surface coefficients for case 2a.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 457 x 191 UKB 67 Steel weight per frame: 2007 kg

This represents a 17% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2b: with the left column subject to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coeff = -0.521/(1.031 x 0.963) = -0.524.

Wind Blowing From	Left	Right	Near	Far	Ŀ
	Left Wall/Co	olumn] [
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1:
Basic Pressure Coefficient	-0.280	-0.524	-0.589	-0.589	14
Factored Pressure Coefficient	-0.278	-0.521	-0.585	-0.585	1
	Right Wall/C	olumn			1
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	1
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497],

Fig 12.3 shows the edited external surface coefficients for case 2b.

Autodesign produces the following sections for this case:



Rafters: 406 x 178 UKB 60 Columns: 457 x 191 UKB 74 Steel weight per frame: 2227 kg

This represents a 30% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The internal suction case 2b therefore governs the design.

3.13 Duopitch portal building with near, far and right sides open

The following text explains the modifications to be made for three adjacent sides open. The procedure is the same but 'handed' for an open near, far and left sides but is given in full in section 3.12 to avoid cross referencing and interpretation. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2:

Wind direction $ heta$	On	e open face	Two adjacent	Three open faces ^a	
	Shorter	Longer	open faces		
0°	+0.85	+0.80	+0.77	+0.60	
90 ^{°ь}	-0.60	-0.46	-0.57	-0.63	
	+0.52	+0.67	+0.77	+0.40	
180°	-0.39	-0.43	-0.60	-0.56	
 a Values given should b b Where two sets of values 	e applied to underside o les are given they shoul	f roof only. For the single d be treated as separate lo	wall, use pressure coefficient ad cases.	s for walls given in Table 5.	

Table 18 — Internal pressure coefficients $C_{\rm pi}$ for open-sided buildings

Attention is drawn to note (a) to the table which applies when the right side is completely open. The implication here is that different internal surface coefficients are applicable to the roof and walls. This does not seem entirely logical and cannot be accommodated in the present version of SMART Portal. However the difference between applying the relevant table 5 and table 18 coefficients to the single wall is marginal and of the same order as the uncertainties implicit in the guidance. Therefore it is proposed to ignore note (a) in the interests of simplicity and practical use of the software.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole left face is open the diagonal dimension is given with sufficient accuracy by:

 $Sqrt{36^2 + 5^2} =$ 36.3 = m а The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: = Ca 0.85 $Sqrt\{6^2 + 5^2\}$ 7.8 If only one bay is open а = m The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km

from the sea: Ca = 0.96

For the purposes of the example let us assume Ca = 0.90

Therefore edit the value of Ca in fig 1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left

This direction equates to 180° in table 18 for which Cpi = -0.56. Therefore edit the default internal suction coefficient from -0.300 to -0.56.



There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients – wind blowing from right

In BS 6399-2 Table 18, right wind equates to wind 0° blowing into the open longer face for which Cpi = 0.60. Therefore edit the default internal pressure coefficient from +0.20 to + 0.60.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients - wind blowing on near end

This direction equates to wind 90° in table 18 for which Cpi = + 0.40 or -0.63. The positive coefficient corresponds to wind blowing into the building at a skew angle so as to attack the inside face of the left wall. The negative coefficient corresponds to wind blowing onto the building at a skew angle so as to attack the outside face of the left wall. Therefore edit the default values +0.20 and -0.30 to +0.40 and -0.63 respectively.

Internal surface coefficients - wind blowing on far end

This direction equates to wind 90° in table 18 for which Cpi = + 0.40 or -0.63. The positive coefficient corresponds to wind blowing into the building at a skew angle so as to attack the inside face of the left wall. The negative coefficient corresponds to wind blowing onto the building at a skew angle so as to attack the outside face of the left wall. Therefore edit the default values +0.20 and -0.30 to +0.40 and -0.63 respectively.

Wind Blowing From	Left	Right	Near	Far	*
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	
Inter	nal Surface Co	efficients			Ξ
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.200	0.600	0.400	0.400	
Factored Pressure Coefficient	0.186	0.557	0.371	0.371	
Basic Suction Coefficient	-0.560	-0.300	-0.630	-0.630	
Factored Suction Coefficient	-0.520	-0.278	-0.585	-0.585	Ŧ

After editing the internal surface coefficients should appear as shown in fig 11 below.

Fig 13.1 Internal surface coefficients after editing for open right, near and far sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open right side. The coefficients for the right side depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the right side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the right column has cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 51 Columns: 406 x 178 UKB 60 Steel weight per frame: 1854 kg



This solution represents an 8% increase over the design for a closed sided building. In other circumstances the difference would be lesser or greater.

At the other extreme a right column may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column, the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying right external surface coefficients equal and opposite to the internal surface coefficients. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients which will also cater for the cases where the wind code provides alternative + and – coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively two versions of the frame can be run:-

Case 2a: with the right column subject to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind right basic coeff = 0.557/(1.031 x 0.963) = 0.561.

Wind Blowing From	Left	Right	Near	Far	
	Left Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500	
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497	
	Right Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	0.187	0.561	0.374	0.374	
Factored Pressure Coefficient	0.186	0.557	0.372	0.372	-

Fig 13.2 Edited external surface coefficients for case 2a.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 457 x 191 UKB 67 Steel weight per frame: 2007 kg

This represents a 17% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

Case 2b: with the right column subject to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic coeff = 0.520/(1.031 x 0.963) = 0.523.



Wind Blowing From	Left	Right	Near	Far	-		
Left Wal/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=		
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500			
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497			
	Right Wall/Co	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.523	-0.280	-0.589	-0.589	1		
Factored Pressure Coefficient	-0.520	-0.278	-0.585	-0.585	-		

Fig 12.3 shows the edited external surface coefficients for case 2b.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The internal suction case 2b therefore governs the design

3.14 Duopitch portal building with near, left and right sides open

The following text explains the modifications to be made for three adjacent sides open. The procedure is the same but 'handed' for an open far, left and right sides but that case is given in full in section 3.15 to avoid cross referencing and interpretation. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2:

Wind direction θ	One	One open face		Three open faces ^a
	Shorter	Longer	open faces	
0°	+0.85	+0.80	+0.77	+0.60
90°ь	-0.60	-0.46	-0.57	-0.63
	+0.52	+0.67	+0.77	+0.40
180°	-0.39	-0.43	-0.60	-0.56

Table 18 — Internal pressure coefficients C_{pi} for open-sided buildings

^a Values given should be applied to underside of roof only. For the single wall, use pressure coefficients for walls given in Table 5.
^b Where two sets of values are given they should be treated as separate load cases.

Attention is drawn to note (a) to the table. The implication here is that different internal surface coefficients are applicable to the roof and the single wall. This does not seem entirely logical and cannot be accommodated in the present version of SMART Portal. However the difference between applying the relevant table 5 and table 18 coefficients to the single wall is marginal and of the same order as the uncertainties implicit in the guidance. Therefore it is proposed to ignore note (a) in the interests of simplicity and practical use of the software.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension a for internal pressure is the diagonal dimension of the open face. In the present example if the whole left or right face is open the diagonal dimension is given with sufficient accuracy by:

a = $Sqrt{36^2 + 5^2}$ = 36.3 m

The corresponding size effect factor can be read from BS 6399-2 fig 4 for a site in country >2 km from the sea: Ca = 0.85



If only one bay is open	а	=	Sqrt{6 ² + 5 ² }	=	7.8	m
The corresponding size effect factor can be re	ead from	BS 6	5399-2 fig 4 for a	site in	country	>2 km
from the sea:	Ca	=	0.96			
For the purposes of the example let us assume	Ca	=	0.90			

Therefore edit the value of Ca in fig 1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left

This direction equates to wind 90° in table 18 for which Cpi = + 0.40 or -0.63. The positive coefficient corresponds to wind blowing into the building at a skew angle so as to attack the inside face of the far wall. The negative coefficient corresponds to wind blowing onto the building at a skew angle so as to attack the outside face of the far wall. Therefore edit the default values +0.20 and -0.30 to +0.40 and -0.63 respectively.

Internal surface coefficients – wind blowing from right

This direction equates to wind 90° in table 18 for which Cpi = + 0.40 or -0.63. The positive coefficient corresponds to wind blowing into the building at a skew angle so as to attack the inside face of the far wall. The negative coefficient corresponds to wind blowing onto the building at a skew angle so as to attack the outside face of the far wall. Therefore edit the default values +0.20 and -0.30 to +0.40 and -0.63 respectively.

Internal surface coefficients - wind blowing from near side

In BS 6399-2 Table 18, near wind equates to wind 0° blowing into the open shorter face for which Cpi = 0.60. Therefore edit the default internal pressure coefficient from +0.20 to + 0.60.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

Internal surface coefficients – wind blowing from far side

This direction equates to 180° in table 18 for which Cpi = -0.56. Therefore edit the default internal suction coefficient from -0.300 to -0.56.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Wind Blowing From	Left	Right	Near	Far	^		
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751			
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1		
Internal Surface Coefficients							
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900			
Basic Pressure Coefficient	0.400	0.400	0.600	0.200			
Factored Pressure Coefficient	0.371	0.371	0.557	0.186	1		
Basic Suction Coefficient	-0.630	-0.630	-0.300	-0.560	1		
Factored Suction Coefficient	-0.585	-0.585	-0.278	-0.520	-		

After editing the internal surface coefficients should appear as shown in fig 14.1 below.

Fig 14.1 Internal surface coefficients after editing for open left, right and near sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open left and right sides. The coefficients for the left and right sides depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the left or right side may be



unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the columns have cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 406 x 178 UKB 60 Steel weight per frame: 1717 kg

This solution is the same as the design for the equivalent closed sided building as given in section 3.1. In other circumstances there may be differences. At the other extreme a left or right column (or both) may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column(s), the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying external surface coefficients equal and opposite to the internal surface coefficients on the relevant columns. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients. Forthcoming versions of the software will provide two sets of external coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively several versions of the frame can be run:-

• Case 2a: Left column without cladding. Right column with cladding. Internal pressure.

The left column is subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.371/(1.031 \times 0.963) = 0.373$.

Wind Blowing From	Left	Right	Near	Far	Ľ		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	117		
Basic Pressure Coefficient	0.373	0.373	0.561	0.187	1 -		
Factored Pressure Coefficient	0.371	0.371	0.557	0.186	1		
	Right Wall/Co	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1		
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	1		
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	-		

Fig 14.2 Edited external surface coefficients for case 2a.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2b: Left column without cladding. Right column with cladding. Internal suction.



The left column is subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.585/(1.031 \times 0.963) = -0.589$.

Wind Blowing From	Left	Right	Near	Far	ŀ		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	11		
Basic Pressure Coefficient	-0.589	0.589	-0.523	-0.280	14		
Factored Pressure Coefficient	-0.585	0.585	-0.520	-0.278	1		
	Right Wall/C	olumn			1		
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1		
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	1		
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	1,		

Fig 14.3 shows the edited external surface coefficients for case 2b.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2c: Left column with cladding. Right column without cladding. Internal pressure.

The right column is subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.371/(1.031 \times 0.963) = 0.373$.

Wind Blowing From	Left	Right	Near	Far	-		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=		
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500			
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497	1		
	Right Wall/Co	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	0.373	0.373	0.557	0.187	1		
Factored Pressure Coefficient	0.371	0.371	0.553	0.186	-		

Fig 14.4 Edited external surface coefficients for case 2c.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2d: Left column with cladding. Right column without cladding. Internal suction.

The right column is subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to



`ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.585/(1.031 \times 0.963) = -0.589$.

Wind Blowing From	Left	Right	Near	Far	ŀ		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500			
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497			
	Right Wall/C	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.589	-0.589	-0.280	-0.524			
Factored Pressure Coefficient	-0.585	-0.585	-0.278	-0.521			

Fig 14.5 shows the edited external surface coefficients for case 2d.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2e: Left column without cladding. Right column without cladding. Internal pressure.

The left and right columns are subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.371/(1.031 \times 0.963) = 0.373$.

Wind Blowing From	Left	Right	Near	Far	-			
Left Wall/Column								
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=			
Basic Pressure Coefficient	0.373	0.373	0.561	0.187				
Factored Pressure Coefficient	0.371	0.371	0.557	0.186				
	Right Wall/Co	olumn						
Size Effect Factor Ca	0.963	0.963	0.963	0.963				
Basic Pressure Coefficient	0.373	0.373	0.561	0.187	1			
Factored Pressure Coefficient	0.371	0.371	0.557	0.186	-			

Fig 14.6 Edited external surface coefficients for case 2e.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The column sizes were increased for member stability.

• Case 2f: Left column without cladding. Right column without cladding. Internal suction.

The left and right columns are subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be



balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.585/(1.031 \times 0.963) = -0.589$.

Wind Blowing From	Left	Right	Near	Far	-		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=		
Basic Pressure Coefficient	-0.589	-0.589	-0.280	-0.524			
Factored Pressure Coefficient	-0.585	-0.585	-0.278	-0.521			
	Right Wall/Co	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.589	-0.589	-0.280	-0.524			
Factored Pressure Coefficient	-0.585	-0.585	-0.278	-0.521	-		

Fig 14.7 Edited external surface coefficients for case 2f.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

For this particular frame configuration the design outcomes may be summarised as follows:-

Ca	se	Rafters	Columns	Weight		
1	Left and right columns clad	356x171UKB45	406x178UKB60	1717	kg	100%
2a,	/b Left unclad right clad	406x178UKB54	533x210UKB82	2182	kg	127%
2c,	d Left clad right unclad	406x178UKB54	533x210UKB82	2182	kg	127%
2e	/f Both sides unclad	356x171UKB45	457x191UKB67	1798	kg	105%
<u> </u>						

Clearly the unsymmetrically clad case is critical.

3.15 Duopitch portal building with far, left and right sides open

The following text explains the modifications to be made for three adjacent sides open. The procedure is the same but `handed' for an open near, left and right sides but that case is given in full in section 3.14 to avoid cross referencing and interpretation. Reference should be made to section 2.6.3 and Table 18 of BS 6399-2:

Wind direction $ heta$	On	e open face	Two adjacent	Three open faces ^a
	Shorter	Longer	open faces	
0°	+0.85	+0.80	+0.77	+0.60
90 ^{°ь}	-0.60	-0.46	-0.57	-0.63
	+0.52	+0.67	+0.77	+0.40
180°	-0.39	-0.43	-0.60	-0.56
 Values given should b Where two sets of values 	e applied to underside o les are given they shoul	f roof only. For the single d be treated as separate lo	wall, use pressure coefficient	s for walls given in Table 5.

Table 18 — Internal pressure coefficients C_{pi} for open-sided buildings

Attention is drawn to note (a) to the table. The implication here is that different internal surface coefficients are applicable to the roof and the single wall. This does not seem entirely logical and



cannot be accommodated in the present version of SMART Portal. However the difference between applying the relevant table 5 and table 18 coefficients to the single wall is marginal and of the same order as the uncertainties implicit in the guidance. Therefore it is proposed to ignore note (a) in the interests of simplicity and practical use of the software.

Internal size effect factor Ca

According to 2.6.3, the relevant dimension (a) for internal pressure is the diagonal dimension of `the open face'. In the present example if the whole left or right face is open the diagonal dimension is given with sufficient accuracy by:

	а	=	$Sqrt{36^2 + 5^2}$	=	36.3	m
The corresponding size effect factor can be re from the sea:	ad from Ca	BS 639 =	9-2 fig 4 for a 0.85	site in	country	>2 km
If only one bay is open	а	=	$Sqrt{6^{2} + 5^{2}}$	=	7.8	m
The corresponding size effect factor can be re from the sea:	ad from Ca	BS 639 =	9-2 fig 4 for a 0.96	site in	country	>2 km
For the purposes of the example let us assume	Са	=	0.90			
Therefore edit the value of Ce in fig 1 should fu	0 720		`			

Therefore edit the value of Ca in fig 1 above from 0.739 to 0.90.

Internal surface coefficients – wind blowing from left

This direction equates to wind 90° in table 18 for which Cpi = + 0.40 or -0.63. The positive coefficient corresponds to wind blowing into the building at a skew angle so as to attack the inside face of the near wall. The negative coefficient corresponds to wind blowing onto the building at a skew angle so as to attack the outside face of the near wall. Therefore edit the default values +0.20 and -0.30 to +0.40 and -0.63 respectively.

Internal surface coefficients – wind blowing from right

This direction equates to wind 90° in table 18 for which Cpi = + 0.40 or -0.63. The positive coefficient corresponds to wind blowing into the building at a skew angle so as to attack the inside face of the near wall. The negative coefficient corresponds to wind blowing onto the building at a skew angle so as to attack the outside face of the near wall. Therefore edit the default values +0.20 and -0.30 to +0.40 and -0.63 respectively.

Internal surface coefficients - wind blowing from near side

This direction equates to 180° in table 18 for which Cpi = -0.56. Therefore edit the default internal suction coefficient from -0.300 to -0.56.

There is no corresponding internal pressure value in table 18 for this wind direction so leave the default value + 0.200 unchanged.

Internal surface coefficients - wind blowing from far side

In BS 6399-2 Table 18, far wind equates to wind 0° blowing into the open shorter face for which Cpi = 0.60. Therefore edit the default internal pressure coefficient from +0.20 to + 0.60.

There is no corresponding suction value for this wind direction so leave the default value -0.30 unchanged.

After editing the internal surface coefficients should appear as shown in fig 15.1 below.



Wind Blowing From	Left	Right	Near	Far	^
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1
Inter	nal Surface Co	efficients			
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.400	0.400	0.200	0.600	
Factored Pressure Coefficient	0.371	0.371	0.186	0.557	1
Basic Suction Coefficient	-0.630	-0.630	-0.560	-0.300	1
Factored Suction Coefficient	-0.585	-0.585	-0.520	-0.278	Ŧ

Fig 15.1 Internal surface coefficients after editing for open left, right and far sides.

External surface coefficients

The external surface coefficients for main frames are unchanged except for the open left and right sides. The coefficients for the left and right sides depend on the situation at the frame being considered for design. As previously noted (in section 2), the whole of the left or right side may be unclad or the opening may be restricted to one or more bays. In this latter case there are clearly two or more wind loading conditions which need to be considered and if necessary justified.

In the current version of SMART Portal 2D it is necessary to run these cases separately.

For the case where the columns have cladding attached both sides (the opening being one or more bays distant), the treatment is simple because the external pressure or suction can co-exist with either internal pressure or suction. The problem reduces to the normal `all sides clad' case with enhanced internal pressures and suctions and no further editing is required. We will refer to this as case 1. Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 406 x 178 UKB 60 Steel weight per frame: 1717 kg

This solution is the same as the design for the equivalent closed sided building given in section 3.1. In other circumstances there may be differences. At the other extreme a left or right column (or both) may have no cladding attached in which case it will attract only negligible wind force. Although this results in lesser direct wind force on the column(s), the overall effect on the frame and the column stability may be critical. We will refer to this as case 2. In principle this case may be modelled by applying external surface coefficients equal and opposite to the internal surface coefficients on the relevant columns. Unfortunately the current versions of SMART Portal provide only one set of external surface coefficients per wind direction which are combined with the two sets of internal coefficients which will also cater for the cases where the wind code provides alternative + and – coefficients for the windward roof slopes. In the meantime it is necessary to exercise some engineering judgement and approximations in order to use the software safely and economically. Alternatively several versions of the frame can be run:-

• Case 2a: Left column without cladding. Right column with cladding. Internal pressure.

The left column is subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.371/(1.031 \times 0.963) = 0.373$.



Wind Blowing From	Left	Right	Near	Far	1	
Left Wall/Column						
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1 =	
Basic Pressure Coefficient	0.371	0.371	0.187	0.561	1	
Factored Pressure Coefficient	0.369	0.369	0.186	0.557	1	
	Right Wall/Co	olumn				
Size Effect Factor Ca	0.963	0.963	0.963	0.963		
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	1	
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497		

Fig 15.2 Edited external surface coefficients for case 2a.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 406 x 178 UKB 60 Steel weight per frame: 1925 kg

This represents a 12% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2b: Left column without cladding. Right column with cladding. Internal suction.

The left column is subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.585/(1.031 \times 0.963) = -0.589$.

Wind Blowing From	Left	Right	Near	Far	^
	Left Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	-0.589	0.589	-0.523	-0.280	
Factored Pressure Coefficient	-0.585	0.585	-0.520	-0.278	
	Right Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	
Basic Pressure Coefficient	-0.500	0.614	-0.800	-0.500	
Factored Pressure Coefficient	-0.497	0.610	-0.795	-0.497	-

Fig 15.3 shows the edited external surface coefficients for case 2b.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2c: Left column with cladding. Right column without cladding. Internal surface.

The right column is subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.371/(1.031 \times 0.963) = 0.373$.



#

Wind Blowing From	Left	Right	Near	Far	Τ			
	Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1			
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500				
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497				
	Right Wall/C	olumn						
Size Effect Factor Ca	0.963	0.963	0.963	0.963	٦.			
Basic Pressure Coefficient	0.373	0.373	0.187	0.561				
Factored Pressure Coefficient	0.371	0.371	0.186	0.557	1			

Fig 15.4 Edited external surface coefficients for case 2c.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 406 x 178 UKB 60 Steel weight per frame: 1925 kg

This represents a 12% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2d: Left column with cladding. Right column without cladding. Internal suction.

The right column is subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.585/(1.031 \times 0.963) = -0.589$.

Wind Blowing From	Left	Right	Near	Far			
	Left Wall/Column						
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=		
Basic Pressure Coefficient	0.614	-0.500	-0.800	-0.500			
Factored Pressure Coefficient	0.610	-0.497	-0.795	-0.497			
	Right Wall/Co	lumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	-0.589	-0.589	-0.524	-0.280			
Factored Pressure Coefficient	-0.585	-0.585	-0.521	-0.278	-		

Fig 15.5 shows the edited external surface coefficients for case 2d.

Autodesign produces the following sections for this case:

Rafters: 406 x 178 UKB 54 Columns: 533 x 210 UKB 82 Steel weight per frame: 2182 kg

This represents a 27% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

• Case 2e: Left column without cladding. Right column without cladding. Internal pressure.

The left and right columns are subjected to external surface coefficients balancing the internal pressure coefficients and deleting all the load combinations with internal suction or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left basic +ve coeff = $0.371/(1.031 \times 0.963) = 0.373$.



Wind Blowing From	Left	Right	Near	Far	P		
Left Wall/Column							
Size Effect Factor Ca	0.963	0.963	0.963	0.963	11		
Basic Pressure Coefficient	0.373	0.373	0.187	0.561	14		
Factored Pressure Coefficient	0.371	0.371	0.186	0.557	1		
	Right Wall/C	olumn					
Size Effect Factor Ca	0.963	0.963	0.963	0.963			
Basic Pressure Coefficient	0.373	0.373	0.187	0.561	1		
Factored Pressure Coefficient	0.371	0.371	0.186	0.557] ,		

Fig 15.6 Edited external surface coefficients for case 2e.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater. The column sizes were increased for member stability.

• Case 2f: Left column without cladding. Right column without cladding. Internal suction.

The left and right columns are subjected to external surface coefficients balancing the internal suction coefficients and deleting all the load combinations with internal pressure or setting them to `ignore'. Note that it is the `factored' internal coefficients which are to be balanced. Enter the value of basic external coefficient = factored internal coefficient /(dynamic augmentation factor x external size factor) In the example for wind left or right basic coeff = $-0.585/(1.031 \times 0.963) = -0.589$.

Wind Blowing From	Left	Right	Near	Far	
	Left Wall/Co	olumn			1 [.
Size Effect Factor Ca	0.963	0.963	0.963	0.963	11
Basic Pressure Coefficient	-0.589	-0.589	-0.524	-0.280	1 -
Factored Pressure Coefficient	-0.585	-0.585	-0.521	-0.278	1
	Right Wall/C	olumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1
Basic Pressure Coefficient	-0.589	-0.589	-0.524	-0.280	1
Factored Pressure Coefficient	-0.585	-0.585	-0.521	-0.278	1.

Fig 15.7 Edited external surface coefficients for case 2f.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This represents a 5% increase over the design for a closed sided building. In other circumstances the difference could be lesser or greater.

For this particular frame configuration the design outcomes may be summarised as follows:-

Case	Rafters	Columns	Frame	weight	
1: Left and right columns clad	356x171UKB45	406x178UKB60	1717	kg	100%
2a/b Left unclad right clad	406x178UKB54	533x210UKB82	2182	kg	127%
2c/d Left clad right unclad	406x178UKB54	533x210UKB82	2182	kg	127%
2e/f Both sides unclad	356x171UKB45	457x191UKB67	1798	kg	105%
Clearly the unsymmetrically cla	d case is critical.				



3.16 Duopitch portal building with all sides partly open

BS 6399-2 does not deal specifically with the case of four sides partly open as defined in section 2 of this guide. However comparison of results for other configurations indicates that for the purpose of designing main portal frames case 11 in this guide may be adopted.

3.17 Duopitch portal building with all sides fully open (canopy)

BS 6399-2 provides guidance for wind effects on free-standing canopies in section 2.5.9.1 and tables 13, 14 and 15. It is important to note that although free-standing canopies are usually designed for full or partial blockage, the blocking object or materials are not connected to the structure and the columns do not sustain any significant wind load from cladding attached thereto. The tables therefore provide coefficients for wind actions on the roof only. The tabulated coefficients are net values of the resultant of pressure/suctions on the upper and lower surfaces of the roof and do not reveal the individual surface contributions which would be helpful for structures with separate soffit cladding and framing such as petrol station canopies. However it is possible to deduce/infer the upper and lower surface values by comparison with the external surface coefficients for closed buildings. For the purpose of this guide we will assume single layer cladding.

It will be observed that many canopies have significant edge or fascia cladding. Clause 2.5.9.1.5 provides force coefficients. It is not possible to model this in the current version of SMART Portal so it is assumed that once a satisfactory design has been obtained the data will be exported to CADS A3D MAX so that fascia loading can be added and the design re-analysed and code-checked. It is planned to add fascia wind loading in a future upgrade of SMART Portal.

The following example is derived from the basic fully clad duopitch building discussed in section 2 of this guide and has the same frame dimensions, dead and imposed loads and dynamic wind pressure.

The roof net pressure/suction coefficients are obtained from Table 14 of BS 6399-2 as shown below:



Pitch angle α	Load case	Overall		Local co	fficients	
		coefficients	Α	В	с	D
-20°	Maximum, all ζ	+0.7	+0.8	+1.6	+0.6	+1.7
	Minimum $\zeta = 0$	-0.7	-0.9	1.3	-1.6	-0.6
	Minimum $\zeta = 1$	-1.5	-1.5	-2.4	-2.4	-1.2
-15°	Maximum, all ζ	+0.5	+0.6	+1.5	+0.7	+1.4
	Minimum $\zeta = 0$	-0.6	-0.8	-1.8	-1.6	-0.6
	Minimum $\zeta = 1$	-1.5	-1.5	-2.7	-2.6	-1.2
-10°	Maximum, all ζ	+0.4	+0.6	+1.4	+0.8	+1.1
	Minimum $\zeta = 0$	-0.6	-0.8	-1.3	-1.5	-0.6
	$\operatorname{Minimum} \zeta = 1$	-1.4	1.4	-2.5	-2.5	-1.2
-5°	Maximum, all ζ	+0.3	+0.5	+1.5	+0.8	+0.8
	$\operatorname{Minimum} \zeta = 0$	-0.5	-0.7	-1.3	-1.6	-0.6
	Minimum $\zeta = 1$	-1.4	-1.4	-2.3	-2.4	-1.2
+5°	Maximum, all ζ	+0.3	+0.6	+1.8	+1.3	+0.4
	$\operatorname{Minimum} \zeta = 0$	-0.6	-0.6	-1.4	-1.4	-1.1
	Minimum $\zeta = 1$	-1.2	-1.2	-2.0	1.8	-1.5
+10°	Maximum, all ζ	+0.4	+0.7	+1.8	+1.4	+0.4
	Minimum $\zeta = 0$	-0.7	-0.7	-1.5	-1.4	-1.4
	Minimum $\zeta = 1$	-1.2	-1.2	-1.8	-1.6	-1.6
+15°	Maximum, all ζ	+0.4	+0.9	+1.9	+1.4	+0.4
	Minimum $\zeta = 0$	0.8	-0.9	-1.7	-1.4	-1.8
	Minimum $\zeta = 1$	-1.2	-1.2	-1.6	-1.3	-1.7
+20°	Maximum, all ζ	+0.6	+1.1	+1.9	+1.5	+0.4
×	Minimum $\zeta = 0$	-0.9	-1.2	-1.8	-1.4	-2.0
	Minimum $\zeta = 1$	-1.2	-1.2	-1.5	-1.2	-1.7
+25°	Maximum, all ζ	+0.7	+1.2	+1.9	+1.6	+0.5
	Minimum $\zeta = 0$	-1.0	-1.4	-1.9	-1.4	-2.0
	Minimum $\zeta = 1$	-1.2	-1.2	-1.4	-1.1	-1.6
+30°	Maximum, all ζ	+0.9	+1.3	+1.9	+1.6	+0.7
	Minimum $\zeta = 0$	-1.0	-1.4	-1.9	-1.4	-2.0
	Minimum $\zeta = 1$	-1.2	-1.2	-1.3	-1.1	-1.6
NOTE 1 Interp	oolation for solidity ratio	may be used in th	e range $0 < \zeta < 1$,			
NOTE 2 Interp	olation for intermediate	pitch angles may	be used hetween v	alues of the same	sign.	
NOTE 3 Load	cases cover all possible w	ind directions. Wh	en using direction	al effective wind a	peeds, use:	
a) these value	s of C_p with the largest	value of V_{e} found;	or			
b) directional	values of C_p from referen	ace [6].				

Table 14 — Net pressure coefficients C_p for free-standing duopitch canopy roofs

Table 14 is illustrated by fig 24 shown below:

For simplicity and conservatively it will be assumed that the canopy may be full blocked at any position.

Clause 2.5.9.1.4 states that "the values in the columns headed `overall coefficients' should be used for the design of members supporting the canopy". This clearly indicates that it is not necessary to apply the local coefficients to the main portal frames. However when read in conjunction with clause 2.5.9.1.3 the status of purlins is ambiguous. Here we are concerned with the main frames only so we will apply the overall coefficients only.

Clause 2.5.9.1.4 also advises that "duopitch canopies should be able to support forces with one slope at the maximum or minimum and the other unloaded."

We will now consider how these loads may be applied in the context of the current functionality of SMART Portal.





As no separate coefficients are given for pressure or suction on the underside of the roof and also the sides are unclad, the internal pressure inputs to the software are redundant so zero values are input in place of the default values as shown below in fig 17.1.

Wind Blowing From	Left	Right	Near	Far	^
Dynamic Pressure (qs)	0.751	0.751	0.751	0.751	
Dynamic Augmentation Factor (1+Cr)	1.031	1.031	1.031	1.031	1
Inter	nal Surface Co	efficients			Ξ
Internal Size Effect Factor Ca	0.900	0.900	0.900	0.900	
Basic Pressure Coefficient	0.000	0.000	0.000	0.000	
Factored Pressure Coefficient	0.000	0.000	0.000	0.000	
Basic Suction Coefficient	0.000	0.000	0.000	0.000	
Factored Suction Coefficient	0.000	0.000	0.000	0.000	Ŧ

Fig 17.1 Internal surface surface coefficients edited for canopy open all sides.



Similarly the external surface coefficients for the left and right columns are set to zero as shown below in fig 17.2.

Wind Blowing From	Left	Right	Near	Far	-
	Left Wall/Co	lumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	=
Basic Pressure Coefficient	0.000	0.000	0.000	0.000	1
Factored Pressure Coefficient	0.000	0.000	0.000	0.000	1
	Right Wall/Co	olumn			
Size Effect Factor Ca	0.963	0.963	0.963	0.963	1
Basic Pressure Coefficient	0.000	0.000	0.000	0.000	1
Factored Pressure Coefficient	0.000	0.000	0.000	0.000	-

Fig 17.2 External surface coefficients for left and right columns edited for canopy open all sides.

The overall coefficients are applied to the roof as shown below in fig 17.3 and 17.4.

Wind Blowing From	Left	Right	Near	Far	•	
Left Roof/Rafter						
Size Effect Factor Ca	0.936	0.936	0.936	0.936		
Basic Main Zone Coefficient	0.300	-1.200	-1.200	0.300		
Basic Edge Zone Coefficient	0.300	-1.200	-1.200	0.300	Ξ	
Edge Zone Width (m)	1.265	1.265	0.000	0.000		
Reduction Factor	1.000	1.000	1.000	1.000		
Factored Main Zone Coefficient	0.289	-1.158	-1.158	0.289		
Factored Edge Zone Coefficient	0.289	-1.158	-1.158	0.289	-	

Fig 17.3 External surface coefficients for left rafter edited for canopy open all sides.

Wind Blowing From	Left	Right	Near	Far	^		
	Right Roof/Rafter						
Size Effect Factor Ca	0.936	0.936	0.936	0.936			
Basic Main Zone Coefficient	0.000	0.000	-1.200	0.300			
Basic Edge Zone Coefficient	0.000	0.000	-1.200	0.300			
Edge Zone Width (m)	1.265	1.265	0.000	0.000			
Reduction Factor	1.000	1.000	1.000	1.000	=		
Factored Main Zone Coefficient	0.000	0.000	-1.158	0.289			
Factored Edge Zone Coefficient	0.000	0.000	-1.158	0.289	-		

Fig 17.4 External surface coefficients for right rafter edited for canopy open all sides.

In the above the following assumptions have been made:

- From table 14 for roof slope 5[°], the maximum and minimum overall net coefficients are +0.30 and -1.20.
- The wind near and far conditions are assumed to produce symmetrical loading on the left and right rafters.
- For wind blowing from the near side the canopy is assumed blocked at the far end leading to maximum uplift with $C_p = -1.2$ on both rafters.
- For wind blowing from the far side the canopy is assumed blocked at the far end leading to suction on the underside and maximum download $C_p = +0.30$ on both rafters.
- For wind blowing from the left side the canopy is assumed blocked on the left side leading to suction on the underside and maximum down load $C_p = +0.30$ on the left rafter. To comply



with clause 2.5.9.1.4 to give maximum unsymmetry the right rafter is somehow not loaded so $C_p = 0.0$.

- For wind blowing from the right side the canopy is assumed blocked on the left side leading to pressure on the underside and external suction so maximum uplift $C_p = -1.20$ on the left rafter. To comply with clause 2.5.9.1.4 to give maximum unsymmetry the right rafter is somehow not loaded so $C_p = 0.0$.
- The optional reduction factors (0.60) applied to clad building surfaces where the effect of the load is beneficial (eg suction on windward slope reduces sway effect) are not applied (set to 1.0)because not relevant.

Autodesign produces the following sections for this case:

Rafters: 356 x 171 UKB 45 Columns: 457 x 191 UKB 67 Steel weight per frame: 1798 kg

This solution 5 % heavier than the design for a closed sided building. However the design outcome may be heavier when fascia wind loads are added.

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4 References

1: Cook, NJ The designer's guide to wind loading of building structures Part 2: static structures. London, Butterworths, 1989.

